Extracting Equations of Motion from Superconducting Circuits

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Alternative computing paradigms open the door to exploiting recent innovations in computational hardware to probe the fundamental thermodynamic limits of information processing. One such paradigm employs superconducting quantum interference devices (SQUIDs) to execute classical computations. This, though, requires constructing sufficiently complex superconducting circuits that support a suite of useful information processing tasks and storage operations, as well as understanding these circuits' energetics. First-principle circuit design, though, leads to prohibitive algebraic complications when deriving the effective equations of motion—complications that to date have precluded achieving these goals, let alone doing so efficiently. We circumvent these complications by (i) specializing our class of circuits and physical operating regimes, (ii) synthesizing existing derivation techniques to suit these specializations, and (iii) implementing solution-finding optimizations which facilitate physically interpreting circuit degrees of freedom that respect physically-grounded constraints. This leads to efficient, practical circuit prototyping and access to scalable circuit architectures. The analytical efficiency is demonstrated by reproducing the potential energy landscape generated by the quantum flux parametron (QFP). We then show how inductively coupling two QFPs produces a device that is capable of executing 2-bit computations via its composite potential energy landscape. More generally, the synthesis methods detailed here provide a basis for constructing universal logic gates and investigating their thermodynamic performance.

I. INTRODUCTION

All computation is physical. To effect information processing, one approach entails a sequence of stochastic transformations that systematically manipulate a system's potential energy landscape [1, 2]. Reliable computing, in particular, then requires stable memory states physically supported by a system's information-bearing degrees of freedom [3]. Energy minima on the landscape provide this dynamical stability. Computation, then, consists of externally controlling the creation, destruction, and location of energy minima. From this perspective, a device's time-dependent potential energy surface guides the emergence of its computational capabilities.

Exploring a superconducting circuit's ability to perform computational operations in this way involves understanding the device's energetics and subsequent dynamical equations of motion [4–8]. Success in using this approach to design candidate devices, though, requires rapidly determining if a given circuit construction is capable of carrying out computations. And this, in turn, demands a framework that can efficiently derive a circuit's equations of motion. To accomplish this, we synthesize several previous approaches, specializing them to a class of circuits of practical interest. The result is a methodology for generating a readily-interpretable Lagrangian and associated equations of motion for a given circuit in terms of its classical degrees of freedom.

The framework's success is demonstrated through two examples. First, we efficiently reproduce the Lagrangian of a quantum flux parametron (QFP) [4, 5, 9–11]. Then, we show how inductively coupling two QFPs produces a device that can execute a range of 2-bit computations.

II. RELATED WORK

The following synthesizes methods from Refs. [12–15]. Its foundations build on Refs. [12, 13], which introduced a network-theoretic approach to electrical circuit analysis and investigated circuits operating in the quantum regime. Ref. [14] introduced an elegant technique for multi-loop circuits to find *irrotational* degrees of freedom. However, it considered only the circuit's quantum Hamiltonian for investigating time-dependent quantities, such as the transition probabilities between energy eigenstates. And, this departs from our goals. Moreover, to avoid cyclic coordinates in the equations of motion, Ref. [14] restricted each circuit loop to have only a single inductor. The following eschews this restriction and, instead, finds optimal solutions for circuits containing more than one inductor in a loop by algebraically eliminating extra degrees of freedom.

Here, we use the resistive capacitive shunted junction (RCSJ) model for each Josephson junction (JJ). Due to this, the dissipative dynamics arising from finite-valued direct current (DC) resistances must be accounted for. To do this, we rely on Ref. [15]'s method that uses the Rayleigh dissipation function [16] to model the circuit's resistive shunts.

Several alternative approaches are available to analyze circuit behaviors in the quantum regime. One common procedure employs number-phase quantization [17, 18], which does not use a network-theoretic approach. Simulations of the quantum dynamics of similar circuits are detailed in Ref. [19]. This all noted, though the SQUIDs employed here are often the basis for quantum computing devices, we concentrate on their behavior in the classical regime to understand their information-bearing degrees of freedom [10, 20]. This also greatly facilitates follow-in investigations of their thermodynamic performance.

Finally, a complementary approach to JJ circuit analysis considers the charge in a loop [21], as opposed to the magnetic flux. However, previous works [20, 22] revealed that varying magnetic flux provides a convenient circuit control method. Consequently, this grounds the following in a flux-focused interpretation of circuit behavior. A generalized approach to the techniques implemented in Ref. [14] considers arbitrary circuit geometries and electromagnetic fields to construct a Hamiltonian [23]. That said, analytical complications that arise from this first-principles framework preclude rapidly and directly characterizing candidate circuit designs.

III. SUPERCONDUCTING CIRCUIT ANALYSIS

First, we obtain the equations of motion for a given circuit. Then, we show how to find coordinate transformations that produce readily interpretable equations of motion in Langevin form.

A. Circuit Equations of Motion

Following Ref. [12], we define a *branch* to be a particular circuit element, whose time dependent *branch flux* is defined by:

$$\phi_b = \phi_b(t)$$
$$\coloneqq \int_{-\infty}^t \mathrm{d}t' \ v_b(t')$$

This is related to the branch voltage $v_b(t)$, the instantaneous voltage across the circuit element, and the *reduced* branch flux $\varphi_b = 2\pi \phi_b/\phi_0$, where ϕ_0 is the flux quantum.

Before proceeding, several assumptions need to be addressed. To begin, all branches within a circuit correspond to either a Josephson junction (JJ) or an inductor. Corresponding variables are subscripted with a J or L, respectively. All JJs are described by the RCSJ model [24, 25], which is characterized by a critical current I_c [7], capacitance C_J , and DC resistance R. Each inductive branch is modeled by an inductance L in parallel with a capacitance C_L satisfying the limit $C_L/C_J \approx 0$. We adopt C_L as an auxiliary variable in a fashion similar to Ref. [14], in that the limit is used at a particular step in the calculations, which is exemplified in Sections IV A and IV B.

Suppose a circuit is constructed with *n* JJs and *m* inductors for a total of N = n + m branches. The branch flux vector $\mathbf{\Phi}_{\rm b} \coloneqq (\phi_{J_1}, \ldots, \phi_{J_n}, \phi_{L_1}, \ldots, \phi_{L_m})^{\mathsf{T}}$ compactly represents all circuit branch fluxes. When computing the potential and equations of motion, we refer to the truncated branch flux vectors $\mathbf{\Phi}_{\rm b_J} \coloneqq (\phi_{J_1}, \ldots, \phi_{J_n})^{\mathsf{T}}$ and $\mathbf{\Phi}_{\rm b_L} \coloneqq (\phi_{L_1}, \ldots, \phi_{L_m})^{\mathsf{T}}$.

The energy stored in the capacitive components is [12]:

$$\mathcal{L}_T = \frac{1}{2} \dot{\mathbf{\Phi}}_{\mathrm{b}}^{\mathsf{T}} \mathbf{C} \dot{\mathbf{\Phi}}_{\mathrm{b}} , \qquad (1)$$

where the dot indicates a time derivative, and the *capacitance* matrix is:

$$\mathbf{C} \coloneqq \operatorname{diag}\left(C_{J_1}, ..., C_{J_n}, C_{L_1}, ..., C_{L_m}\right) \,.$$

Since we assume that all branches are either inductors or JJs, the energy stored in the inductive elements can be calculated using only Φ_{b_L} . The $m \times m$ inductance matrix **L** denotes the circuit's linear inductances, with diagonal entries corresponding to self-inductances L_i and off-diagonal entries corresponding to the mutual inductive coupling $-M_{ij}$ between L_i and $L_{j\neq i}$. The energy stored in the inductive components is given by [12]:

$$\mathcal{L}_L = \frac{1}{2} \mathbf{\Phi}_{b_L}^{\mathsf{T}} \mathbf{L}^{-1} \mathbf{\Phi}_{b_L} \ . \tag{2}$$

Up to a constant, the JJ potential energy contribution is [12]:

$$\mathcal{L}_J = -\sum_{i=1}^n E_i \cos\left(\frac{2\pi}{\phi_0} \Phi_{\mathrm{b}_J i}\right) , \qquad (3)$$

in which $E_i = (\phi_0/2\pi)I_c$ is the Josephson energy of the *i*th JJ in a circuit.

Equations (2)-(3) together give the circuit's conservative potential energy $\mathcal{L}_V \coloneqq \mathcal{L}_J + \mathcal{L}_L$. Given a physical circuit consisting of inductors and JJs as described above, the circuit Lagrangian $\mathcal{L} \coloneqq \mathcal{L}_T - \mathcal{L}_V$ is, up to a constant:

$$\mathcal{L} = \frac{1}{2} \dot{\Phi}_{\mathrm{b}}^{\mathsf{T}} \mathbf{C} \dot{\Phi}_{\mathrm{b}} - \frac{1}{2} \Phi_{\mathrm{b}_{\mathrm{L}}}^{\mathsf{T}} \mathbf{L}^{-1} \Phi_{\mathrm{b}_{\mathrm{L}}} + \sum_{i=1}^{n} E_{i} \cos\left(\frac{2\pi}{\phi_{0}} \Phi_{\mathrm{b}_{\mathrm{J}}i}\right) .$$
(4)

The nonconservative dissipation from the finite JJ resistive shunts are taken into account by the Rayleigh dissipation function \mathcal{D} , and further incorporated into the Euler-Lagrange equations of motion [15, 16] in terms of a generalized coordinate q_i , as:

$$\frac{\mathrm{d}}{\mathrm{d}t}\frac{\partial \mathcal{L}}{\partial \dot{q}_i} - \frac{\partial \mathcal{L}}{\partial q_i} = -\frac{\partial \mathcal{D}}{\partial \dot{q}_i} , \qquad (5)$$

with

J

$$\mathcal{D} := \sum_{i=1}^{n} \frac{1}{2R_i} (\dot{\phi}_{J_i})^2 .$$
 (6)

 \mathcal{D} accounts for the dissipated power in each JJ branch due to its shunt resistance R_i in terms of its branch flux ϕ_{J_i} . Recalling that only JJ branches have DC resistance values, we rewrite Eq. (6) as:

$$\mathcal{D} = \frac{1}{2} \dot{\boldsymbol{\Phi}}_{\mathrm{b}_{\mathrm{J}}}^{\mathsf{T}} \mathbf{D}^{-1} \dot{\boldsymbol{\Phi}}_{\mathrm{b}_{\mathrm{J}}}$$

whereby, following the same logic as with \mathbf{L}^{-1} , \mathbf{D} has dimensions of $n \times n$. However, unlike \mathbf{L} , \mathbf{D} is manifestly diagonal.

To conclude, we add the contribution of the DC resistances' thermal noise current to the equations of motion via:

$$\frac{\mathrm{d}}{\mathrm{d}t}\frac{\partial\mathcal{L}}{\partial\dot{q}_i} - \frac{\partial\mathcal{L}}{\partial q_i} = -\frac{\partial\mathcal{D}}{\partial\dot{q}_i} + \eta_i(t) , \qquad (7)$$

in which $\eta_i(t)$ is nonzero for the JJ branches only. As is standard in Langevin treatments [10], $\eta_i(t)$ are statistically independent of each other, delta correlated over time, and determined by the fluctuation-dissipation theorem through the relation:

$$\langle \eta_i(t)\eta_j(t')\rangle = \frac{2k_BT}{R_i}\delta_{ij}\delta(t-t') \;.$$

B. Determining Optimal Coordinates

Despite the fact that Eq. (5) marginally accommodates the circuit's topology, it does not account for fluxoid quantization conditions [12, 26]: These require that the sum of the branch fluxes around any loop equals the external flux threading the loop. As a result, while there may appear to be N = n + m degrees of freedom in the Lagrangian, there are only N - F degrees of freedom in a circuit with F independent loops—i.e., loops that contain no other loops—threaded by external fluxes.

In view of this, the external flux vector $\mathbf{\Phi}_{\mathbf{x}} := (\phi_{\mathbf{x}_1}, ..., \phi_{\mathbf{x}_F})^{\mathsf{T}}$ is defined to cast fluxoid quantization into matrix form [14]:

$$\mathbf{\Phi}_{\mathrm{x}} = \mathbf{R} \mathbf{\Phi}_{\mathrm{b}}$$

The $F \times N$ matrix **R** is constructed in such a way that its elements R_{ij} satisfy the following criteria: Let L_i denote the *i*th loop threaded by the external flux Φ_{xi} that may contain branch flux ϕ_j . Then:

$$R_{ij} := \begin{cases} +1 & \phi_j \in \mathsf{L}_i \text{ same orientation as } \Phi_{\mathsf{x}i} \text{ ,} \\ -1 & \phi_j \in \mathsf{L}_i \text{ opposite orientation as } \Phi_{\mathsf{x}i} \text{ , and} \\ 0 & \phi_j \notin \mathsf{L}_i \text{ .} \end{cases}$$

Finally, the circuit's degrees of freedom are defined as $\tilde{\mathbf{\Phi}} := (\tilde{\phi}_1, \ldots, \tilde{\phi}_{N-F})^{\mathsf{T}}$ [14]. Generally, these are a tobe-determined linear combination of the branch fluxes represented by the $(N - F) \times N$ matrix **M**:

$$\widetilde{\mathbf{\Phi}} = \mathbf{M} \mathbf{\Phi}_{\mathrm{b}}$$

Furthermore, due to fluxoid quantization, no more than N-F degrees of freedom in the circuit are expected. The quantization conditions are included by employing the $N \times 1$ augmented flux vector $\tilde{\Phi}_+$ and the $N \times N$ augmented matrix \mathbf{M}_+ [14]:

$$egin{aligned} & \widetilde{\Phi}_+ \coloneqq \begin{pmatrix} \widetilde{\Phi} \\ & \Phi_x \end{pmatrix} \ , \ & \mathbf{M}_+ \coloneqq \begin{pmatrix} \mathbf{M} \\ & \mathbf{R} \end{pmatrix} \ . \end{aligned}$$

Note that the branch flux vector and the augmented flux vector are directly related to each other through \mathbf{M}_+ by:

$$\tilde{\mathbf{\Phi}}_{+} = \mathbf{M}_{+} \mathbf{\Phi}_{\mathrm{b}} \ . \tag{8}$$

With this, the circuit Lagrangian and associated equations of motion can be written in terms of $\tilde{\Phi}_+$ by substituting $\Phi_{\rm b} = \mathbf{M}_+^{-1} \tilde{\Phi}_+$ into Eq. (5). Specifically, to find the circuit's Lagrangian in terms of $\tilde{\Phi}_+$, \mathbf{M}_+ must be invertible. Provided that the columns of \mathbf{M} are chosen to be linearly independent of each other and of the columns of \mathbf{R} , the nonsingularity of \mathbf{M}_+ is guaranteed.

However, ambiguity remains in defining the elements of **M**. Following Ref. [14], these degrees of freedom are deemed *irrotational* by ensuring that they satisfy the following constraint:

$$\mathbf{R}\mathbf{C}^{-1}\mathbf{M}^{\mathsf{T}} = \mathbf{0} \ . \tag{9}$$

This guarantees that the Lagrangian, when written in terms of $\tilde{\Phi}_+$, does not depend on $\dot{\Phi}_x$. Due to this, $\tilde{\Phi}$ is referred to as the *irrotational flux* vector, and $\tilde{\Phi}_+$ is the *augmented irrotational flux* vector. In addition, Eq. (9) allows the equations of motion to be of Langevin form, further enabling thermodynamical analyses of the circuit's degrees of freedom—the subject of a sequel.

However, even after enforcing the irrotational constraint, there is still additional freedom in defining **M**. To address this, we turn to the kinetic energy term:

$$\mathcal{L}_T = \frac{1}{2} \dot{\mathbf{\Phi}}_{\mathrm{b}}^{\mathsf{T}} \mathbf{C} \dot{\mathbf{\Phi}}_{\mathrm{b}} \tag{10}$$

$$= \dot{\tilde{\Phi}}_{+}^{\dagger} (\mathbf{M}_{+}^{-1})^{\mathsf{T}} \mathbf{C} \mathbf{M}_{+}^{-1} \dot{\tilde{\Phi}}_{+}$$
$$= \frac{1}{2} \dot{\tilde{\Phi}}_{+}^{\mathsf{T}} \mathbf{C}_{\text{eff}} \dot{\tilde{\Phi}}_{+} , \qquad (11)$$

in which \mathbf{C}_{eff} is the *effective capacitive* matrix. With Eq. (11) in mind, recall that the goal is to obtain an easily interpretable Lagrangian and corresponding equations of motion for a given circuit. A diagonal \mathbf{C}_{eff} allows for a straightforward interpretation of \mathcal{L}_T as the kinetic energy in both the $\mathbf{\Phi}_{\text{b}}$ and the $\tilde{\mathbf{\Phi}}$ bases. In other words, the task is to find solutions of \mathbf{M} that yield a diagonal \mathbf{C}_{eff} .

Analyzing a number of cases established a set of calculational guidelines that result in a diagonal C_{eff} when solving for the components of **M** through Eq. (9). These aid in the task of finding optimal solutions in the continuous family of possible solutions:

- 1. The first *n* rows of **M** can each contain up to *n* nonzero entries corresponding to the *n* JJ coefficients of $\mathbf{M}\Phi_{\rm b}$, which will have the same magnitude. The other *m* inductive elements of **M**, corresponding to the inductive coefficients in each of these rows, will either be zero or proportional to C_L/C_J ; the latter subsequently vanishes when $C_L/C_J \rightarrow 0$. Note that this limit is taken after a solution is found
- solution is found. 2. When m - F > 0, the last m - F rows of **M** will each contain up to m nonzero entries corresponding to the m inductive flux coefficients of $\mathbf{M}\boldsymbol{\Phi}_{\mathrm{b}}$, which also have the same magnitude. All n JJ coefficients in these rows will contain zero entries, and all nonzero inductive coefficients are unity herein.

Importantly, linear independence between rows must be maintained when implementing these conditions.

To briefly illustrate guideline (1), one possible realization is that in each of the n rows, every JJ coefficient takes on a nonzero value only once, while all other JJ coefficients are zero. If each nonzero value is unity, this is equivalent to there being no coordinate transformation between these branch and irrotational flux coordinates.

Guideline (2) stems from a mismatch between the number of loops and inductors. For example, if m = 2 and F = 1 such that m - F = 1—i.e., there is one loop that contains more than one inductor—this requires setting all JJ coefficients to zero for one solution of Eq. (9). This reflects the over-determination of the additional inductor's behavior in the circuit. Consequently, one cyclic coordinate will appear in the circuit Lagrangian: This can be eliminated through determining its equation of motion and subsequently rewriting it in terms of noncyclic irrotational degrees of freedom. Sections IV A and IV B demonstrate this procedure. Note that if m - F = 0, then guideline (2) does not apply. Additionally, if m - F < 0, finding a diagonal C_{eff} is not possible.

Once the elements of \mathbf{M} are determined, the dynamical degrees of freedom are interpreted as the irrotational degrees of freedom that are not cyclic [16]. Numerically, there are N - F - (m - F) = n, as there will be N - Firrotational flux coordinates with m - F expected to be cyclic. For a multi-loop circuit (F > 1), a diagonal \mathbf{C}_{eff} is found only when there are no more JJs than there are irrotational degrees of freedom. Equivalently, the number of inductors in a circuit containing both JJs and inductors must satisfy $m \ge F$. These conditions can also be explained as the following: Each JJ must be physically represented by at least one dynamical degree of freedom, and there must be at least one inductor per independent circuit loop to capture the circuit flux behavior. Below, we illustrate these conditions by example.

IV. EXAMPLE DEVICE DESIGNS

The following demonstrates how to find the independent information-bearing degrees of freedom via two examples: A quantum flux parametron (QFP) and a device comprised of two inductively coupled QFPs capable of implementing a range of 2-bit computations.

A. Quantum Flux Parametron

We first consider a circuit whose names and constructions span multiple use cases over a number of decades. Figure 1 displays a circuit whose original name was the variable β radio-frequency SQUID [4, 5, 10], and was later known as the compound Josephson junction radiofrequency SQUID [11, 27]. The device's primary use cases involved investigating macroscopic quantum phenomenon, which deviates fundamentally from our goals. Applications that utilize the quantum flux parametron (QFP) [9, 28, 29] align more closely with our goals employing superconducting devices for classical information processing—although the QFP construction differs from that of Refs. [4, 5, 10]. With this considered, we refer to the circuit in Fig. 1 as a QFP.



FIG. 1. A QFP with N = 5 and F = 2. Slight adjustments are made to the physical construction of the circuit to compare to Ref. [5].

Now, the goal is to reproduce the Lagrangian of the circuit shown in Fig. 1—whose design is detailed in Ref. [5]—using the methods detailed in Sections III A and III B. To accomplish this, first we begin writing out the flux vectors:

$$\begin{split} \boldsymbol{\Phi}_{\mathrm{b}} &= \left(\phi_{J_{1}} \ \phi_{J_{2}} \ \phi_{L} \ \phi_{l_{1}} \ \phi_{l_{2}}\right)^{\mathsf{T}} ,\\ \boldsymbol{\Phi}_{\mathrm{b}_{\mathrm{J}}} &= \left(\phi_{J_{1}} \ \phi_{J_{2}}\right)^{\mathsf{T}} ,\\ \boldsymbol{\Phi}_{\mathrm{b}_{\mathrm{L}}} &= \left(\phi_{L} \ \phi_{l_{1}} \ \phi_{l_{2}}\right)^{\mathsf{T}} ,\\ \boldsymbol{\tilde{\Phi}}_{+} &= \left(\widetilde{\phi}_{1} \ \widetilde{\phi}_{2} \ \widetilde{\phi}_{3} \ \phi_{\mathrm{x}_{1}} \ \phi_{\mathrm{x}_{2}}\right)^{\mathsf{T}} .\end{split}$$

With every branch orientation in Fig. 1 pointing upwards, fluxoid quantization gives:

$$\mathbf{R} = \begin{pmatrix} 1 & 0 & -1 & 1 & 0 \\ -1 & 1 & 0 & -1 & 1 \end{pmatrix} \; ,$$

where each row's entries correspond to the column orientation of (J_1, J_2, L, l_1, l_2) , and each row coincides with the external flux loops (ϕ_{x_1}, ϕ_{x_2}) , respectively. Next, the capacitance matrix is written as:

$$\mathbf{C}^{-1} = \operatorname{diag}(C_{J_1}^{-1}, C_{J_2}^{-1}, C_L^{-1}, C_{l_1}^{-1}, C_{l_2}^{-1}) \; .$$

To satisfy Eq. (9), let:

$$\mathbf{M}^{\mathsf{T}} = \begin{pmatrix} M_{11} & M_{21} & M_{31} \\ M_{12} & M_{22} & M_{32} \\ M_{13} & M_{23} & M_{33} \\ M_{14} & M_{24} & M_{34} \\ M_{15} & M_{25} & M_{35} \end{pmatrix} .$$

Then, with the assumption that $C_l \coloneqq C_{l_1} = C_{l_2} = C_L$ and $C_J \coloneqq C_{J_1} = C_{J_2}$, each column of \mathbf{M}^{T} satisfies:

$$CM_{i1} = M_{i3} - M_{i4}$$
 (12)

$$C(M_{i2} - M_{i1}) = M_{i4} - M_{i5}$$
, (13)

with $C \coloneqq C_l/C_J$ and i = 1, 2, 3. From here, we use the guidelines described in Sec. III B to obtain a diagonal C_{eff} . This is achieved first via guideline (1) for the first n = 2 rows of **M** and guideline (2) for the last m - F = 1 row of **M**. We then write a subset of the solution space of Eqs. (12)-(13) into the augmented matrix:

$$\mathbf{M}_{+} = \begin{pmatrix} \mathbf{M} \\ \mathbf{R} \end{pmatrix}$$
$$= \begin{pmatrix} 1/2 & 1/2 & C/4 & -C/4 & -C/4 \\ -1 & 1 & 0 & C & -C \\ 0 & 0 & 1 & 1 & 1 \\ 1 & 0 & -1 & 1 & 0 \\ -1 & 1 & 0 & -1 & 1 \end{pmatrix} , \qquad (14)$$

Consequently, we expect there to be m - F = 1 cyclic irrotational degree of freedom once the circuit Lagrangian \mathcal{L} is found. Next, taking the limit $C \to 0$ and then inverting \mathbf{M}_+ yields:

$$\mathbf{M}_{+}^{-1} = \begin{pmatrix} 1 & -1/2 & 0 & 0 & 0\\ 1 & 1/2 & 0 & 0 & 0\\ 2/3 & 0 & 1/3 & -2/3 & -1/3\\ -1/3 & 1/2 & 1/3 & 1/3 & -1/3\\ -1/3 & -1/2 & 1/3 & 1/3 & 2/3 \end{pmatrix} , \quad (15)$$

which aids in computing the effective capacitive matrix as:

which is diagonal as expected due to following guidelines (1) and (2).

As there are no mutual inductance couplings, the inductance matrix is:

$$\mathbf{L} = \begin{pmatrix} L & 0 & 0 \\ 0 & l_1 & 0 \\ 0 & 0 & l_2 \end{pmatrix}$$

Recalling Eq. (8), and writing the circuit Lagrangian from Eq. (4) in terms of irrotational branch fluxes, produces:

$$\mathcal{L} = \frac{C_J}{2} \left(2 \dot{\widetilde{\phi}}_1^2 + \frac{1}{2} \dot{\widetilde{\phi}}_2^2 \right)$$

$$- \frac{1}{9L} \left(2 \widetilde{\phi}_1 + \widetilde{\phi}_3 - 2 \phi_{x_1} - \phi_{x_2} \right)^2$$

$$- \frac{1}{9l_1} \left(- \widetilde{\phi}_1 + \frac{3}{2} \widetilde{\phi}_2 + \widetilde{\phi}_3 + \phi_{x_1} - \phi_{x_2} \right)^2$$

$$- \frac{1}{9l_2} \left(- \widetilde{\phi}_1 - \frac{3}{2} \widetilde{\phi}_2 + \widetilde{\phi}_3 + \phi_{x_1} + 2 \phi_{x_2} \right)^2$$

$$+ E_{2+1} \cos \widetilde{\varphi}_1 \cos \frac{\widetilde{\varphi}_2}{2} - E_{2-1} \sin \widetilde{\varphi}_1 \sin \frac{\widetilde{\varphi}_2}{2} , \quad (16)$$

where $E_{2\pm 1} = E_{J_2} \pm E_{J_1}$.

The Lagrangian is independent of ϕ_3 which indicates that it is, as expected, a cyclic degree of freedom: It can be eliminated by computing the Euler-Lagrange equation of motion, finding that $\phi_3 = \phi_1 - \phi_{x_1} - \phi_{x_2}/2$, and substituting this into \mathcal{L} . A map between the circuit flux variables in Eq. (16) and those from Ref. [5] can then be identified as:

$$\begin{split} \phi_1 &= \phi \ ,\\ \phi_2 &= \phi_{\rm dc} \ ,\\ \phi_{\rm x_1} &= \phi_{\rm x} - \frac{1}{2} \phi_{\rm xdc} \ , \ {\rm and} \\ \phi_{\rm x_2} &= \phi_{\rm xdc} \ . \end{split}$$

Making these substitutions into Eq. (16) yields a Lagrangian \mathcal{L} that matches that of Ref. [5] with the preceding variable substitutions:

$$\mathcal{L} = \mathcal{L}_T - \mathcal{L}_{\mathrm{v}\beta\text{-rf}}$$
(17)
$$= \frac{C_J}{2} \left(2\dot{\phi}^2 + \frac{1}{2}\dot{\phi}_{\mathrm{dc}}^2 \right)$$
$$- \frac{1}{2L} (\phi - \phi_{\mathrm{x}})^2 - \frac{1}{2l} (\phi_{\mathrm{dc}} - \phi_{\mathrm{xdc}})^2$$
$$+ E_{2+1} \cos\varphi \cos\frac{\varphi_{\mathrm{dc}}}{2} - E_{2-1} \sin\varphi \sin\frac{\varphi_{\mathrm{dc}}}{2} .$$

B. Inductively Coupled QFPs

For our final example, consider inductively coupling two QFPs through L_1 and L_2 via the mutual inductance coupling constant $M \coloneqq M_{12} = M_{21}$, shown in Fig. 2. Using the methods described in Secs. III A and III B, as well as the results from Sec. IV A, allows rapidly deriving its potential. After this, we discuss how this controllable potential performs 2-bit computations.

The choice of branch orientation for the circuit in Fig. 2 is represented by:

$$\mathbf{R} = \begin{pmatrix} 1 & 0 & 0 & 0 & -1 & 0 & 1 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 & 0 & 0 & -1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & -1 & 0 & 0 & 1 & 0 \\ 0 & 0 & -1 & 1 & 0 & 0 & 0 & 0 & -1 & 1 \end{pmatrix} \ ,$$



FIG. 2. Two QFPs inductively coupled via *M*: A superconducting device that supports 2-bit classical computations through the manipulation of its potential energy landscape.

in which each row's elements coincide with the column orientation $(J_1, J_2, J_3, J_4, L_1, L_2, l_1, l_2, l_3, l_4)$, each row corresponds to the external flux loop $(\phi_{1x}, \phi_{1xdc}, \phi_{2x}, \phi_{2xdc})$, and each branch orientation of the upper [lower] SQUID points left [right]. Using the irrotational constraint $\mathbf{RC}^{-1}\mathbf{M}^{\mathsf{T}} = \mathbf{0}$, we find that the elements of \mathbf{M} need to satisfy:

$$CM_{i1} = M_{i5} - M_{i7}$$
$$C(M_{i2} - M_{i1}) = M_{i7} - M_{i8}$$
$$CM_{i3} = M_{i6} - M_{i9}$$
$$C(M_{i4} - M_{i3}) = M_{i9} - M_{i10}$$

Taking a lesson from the single QFP case, and after taking $C \rightarrow 0$, our choice of **M** and **R** leads to:

whose inverse is:

We then eliminate the cyclic degrees of freedom ϕ_5 and ϕ_6 . Following the single QFP case detailed in Sec. IV A, the map between our flux variables and those of Ref. [5] is:

$$\begin{split} \widetilde{\phi}_i &= \phi_j \ ,\\ \widetilde{\phi}_{i+1} &= \phi_{j\mathrm{dc}} \ ,\\ \phi_{\mathbf{x}_i} &= \phi_{j\mathbf{x}} - \frac{1}{2}\phi_{j\mathrm{xdc}} \ , \ \mathrm{and} \\ \phi_{\mathbf{x}_{i+1}} &= \phi_{j\mathrm{xdc}} \ . \end{split}$$

Here, the index *i* corresponds to either the *i*th dynamical degree of freedom or the *i*th external flux, while the index j aligns with the flux in the *j*th QFP, for which i = 1, 3 and j = 1, 2, respectively.

Next, the inductive contribution to the potential, when taking $L := L_1 = L_2$ and $l := l_1 = l_2 = l_3 = l_4$, is found by first writing:

$$\mathbf{L} = \begin{pmatrix} L & -M & 0 & 0 & 0 & 0 \\ -M & L & 0 & 0 & 0 & 0 \\ 0 & 0 & l & 0 & 0 & 0 \\ 0 & 0 & 0 & l & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & l \end{pmatrix} \,.$$

Then, subsequently taking its inverse gives:

$$\mathbf{L}^{-1} = \begin{pmatrix} 1/L_{\alpha} & \mu/L_{\alpha} & 0 & 0 & 0 & 0 \\ \mu/L_{\alpha} & 1/L_{\alpha} & 0 & 0 & 0 & 0 \\ 0 & 0 & 1/l & 0 & 0 & 0 \\ 0 & 0 & 0 & 1/l & 0 & 0 \\ 0 & 0 & 0 & 0 & 1/l & 0 \\ 0 & 0 & 0 & 0 & 0 & 1/l \end{pmatrix} \,,$$

where $L_{\alpha} = \alpha L$, $\alpha = 1 - \mu^2$, and $\mu = M/L$. With this, the potential is then:

$$\mathcal{L}_{V} = -E_{2+1}\cos\varphi_{1}\cos\frac{\varphi_{1dc}}{2} + E_{2-1}\sin\varphi_{1}\sin\frac{\varphi_{1dc}}{2} - E_{4+3}\cos\varphi_{2}\cos\frac{\varphi_{2dc}}{2} + E_{4-3}\sin\varphi_{2}\sin\frac{\varphi_{2dc}}{2} + \frac{1}{2l}(\phi_{1dc} - \phi_{1xdc})^{2} + \frac{1}{2l}(\phi_{2dc} - \phi_{2xdc})^{2} + \frac{1}{2L_{\alpha}}(\phi_{1} - \phi_{1x})^{2} + \frac{1}{2L_{\alpha}}(\phi_{2} - \phi_{2x})^{2} + \frac{\mu}{L_{\alpha}}(\phi_{1} - \phi_{1x})(\phi_{2} - \phi_{2x}) .$$
(18)

If we assume small coupling by keeping only linear terms in μ , then $L_{\alpha}^{-1} \rightarrow L^{-1}$, resulting in Eq. (18) simplifying to a sum of two QFPs potential contributions and a mutual inductance coupling $\mathcal{L}_{M.I.}$:

$$\mathcal{L}_{V} = \mathcal{L}_{\mathrm{v\beta-rf}\ 1} + \mathcal{L}_{\mathrm{v\beta-rf}\ 2} + \mathcal{L}_{\mathrm{M.I.}} , \qquad (19)$$

in which $\mathcal{L}_{M.I.} = \mu (\phi_1 - \phi_{1x}) (\phi_2 - \phi_{2x}) / L.$

A two dimensional projection of Eq. (19) is shown in Fig. 3: The potential has four stable energy minima which can each be assigned a computational memory state—00, 01, 10, and 11. Taking advantage of the metastable regions near each minimum, we can store information. By varying the values of M, ϕ_{ix} and ϕ_{ixdc} for which i = 1, 2, we can process that information—using the dynamics of the Euler-Lagrange equation of motion to implement 2-bit logic gates. Note that while we considered M to be a tunable coupling constant, the details of its construction—a SQUID coupler—are detailed in Refs. [27, 30, 31], whose equations of motion could be accounted for within the complete device construction if its dynamics become important in future investigations.

V. CONCLUSION

We introduced a superconducting circuit methodology that enables exploring the classical informational processing properties of a candidate superconducting circuit through understanding the circuit's energetics and subsequent dynamics. The methods reproduce—in an analytically efficient way—potentials used for experimentally investigating information-bearing degrees of freedom [20], as well as constructing a device that supports 2-bit computations. A sequel describes the information processing properties and energetic performance in detail.

This is the first effort in a series on physically-realizable classical computing. In point of fact, the coupled QFPs shown in Fig. 2 also supports the information processing behavior exhibited by a Szilard engine [1, 32, 33]. Follow-on efforts explore the dynamical and thermodynamic properties of these circuits and implement universal gates—e.g., NAND, NOR, and Fredkin.



FIG. 3. Example potential energy landscape generated by Eq. (19). Instantiating each region surrounding an energy minimum as a computational memory state—00, 10, 01, and 11—permits information storage. Information processing is accomplished by way of a control protocol that employs the mutual inductance and external flux parameters to transform the landscape.

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